

Gasification of RDF in two-stage reactor unit, comparison of two reactor configurations

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Introduction

- RDF Refuse derived fuel
- Gasification syngas production
- Tars undesired product

RDF characterisation

| Ultimate analysis (wt. %) | | Proximate analysis (wt. %) | | | | |
|------------------------------|------|-------------------------------|------|--|--|--|
| N | 1,4 | Ash | 10 | | | |
| C | 52 | Moisture | 4 | | | |
| Н | 8,2 | Volatile matters | 81 | | | |
| S | 0,22 | Fixed carbon | 6 | | | |
| 0 | 28 | | | | | |
| Cl | 0,72 | LHV (MJ/kg) | 21,3 | | | |



Goals

Comparison of 2 reactor configurations

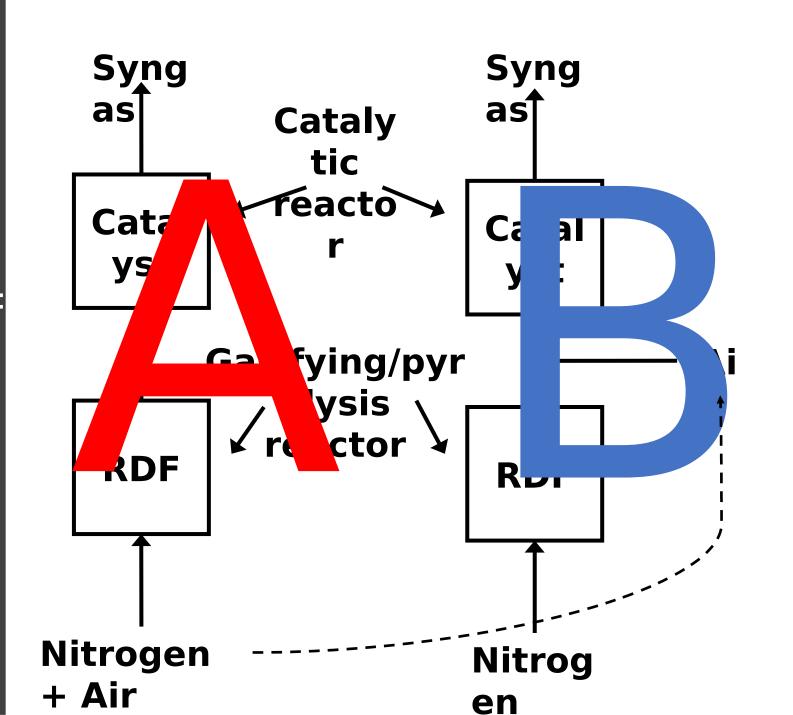
- Syngas composition
- Tar yields

Materials and methods

Idea: partial oxidation zone:
air + volatiles = high
temperature

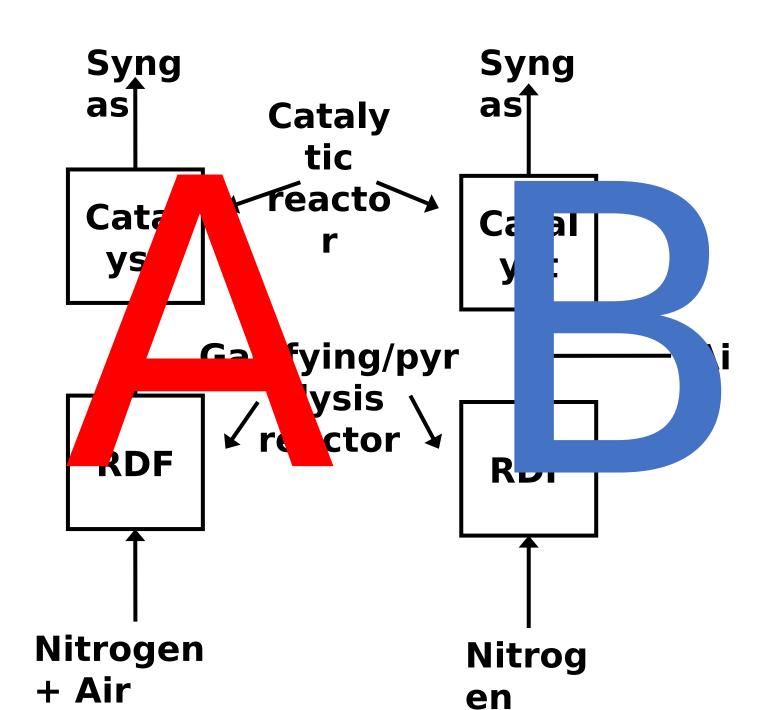
=> lower tar content in syngas

Configuration A Configuration B

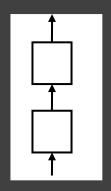


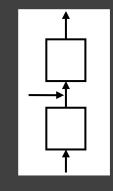
Materials and methods

- Semibatch process: 10 g sample of RDF, 10 g catalyst, 15 L/h N_2 , 10 L/h air.
- Operating conditions: temperature of reactors – 700, 750 and 800 °C, preheated catalytic reactor, preheated furnace for gasifying/pyrolysis reactor.
- Catalyst: clay based catalyst enhanced by nickel oxide
- Syngas composition (sampled at the 5th minute)
- Tar yields determined by vacuum



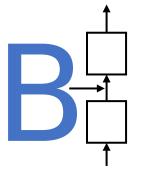
Results





| | Configuration A | | | Configuration B | | | | | | |
|--------------------------|-----------------|------|------|-----------------|------|------|--|--|--|--|
| Temperature | | | | | | | | | | |
| (°C) | 700 | 750 | 800 | 700 | 750 | 800 | | | | |
| Gas Composition (vol. %) | | | | | | | | | | |
| CO ₂ | 38,8 | 38,7 | 36,9 | 40,9 | 27,1 | 17,3 | | | | |
| H ₂ | 27,8 | 25,0 | 18,2 | 24,5 | 31,2 | 41,0 | | | | |
| СО | 11,2 | 17,6 | 35,1 | 11,4 | 17,0 | 34,0 | | | | |
| Methane | 8,2 | 4,8 | 3,0 | 11,5 | 11,1 | 4,6 | | | | |
| Hydrocarbons | 14,0 | 14,0 | 6,9 | 12,4 | 13,7 | 2,9 | | | | |
| | | | | | | | | | | |
| Tar yields [mg/g RDF] | 15,4 | 14,4 | 9,19 | 15,5 | 14,4 | 5,61 | | | | |

Conclusion



- Effect of partial oxidation on tar yields was obscured by activity of catalyst at 700 °C and 750 °C
- At 800 °C was observed drop of tar yield (comparison of configurations) and CO₂ and increased volume content of H₂
- Nickel oxide reduction by H₂
- H₂/CO ratio above 2 at 700 °C
- Pyrolysis coke utilisation

Thank you for your attention